Vehicle-Track Interaction & Dynamics

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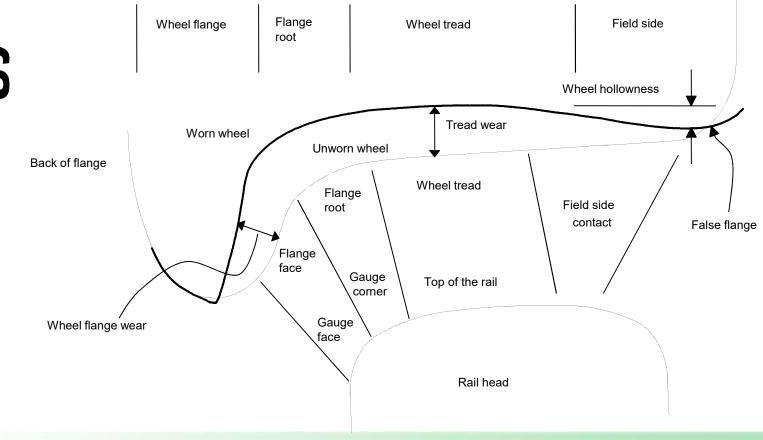


Agenda

- 1. Vehicle steering, stability and curving forces
- 2. Wheel-rail profile design and performance
- 3. VTI derailment mechanisms and risk assessment









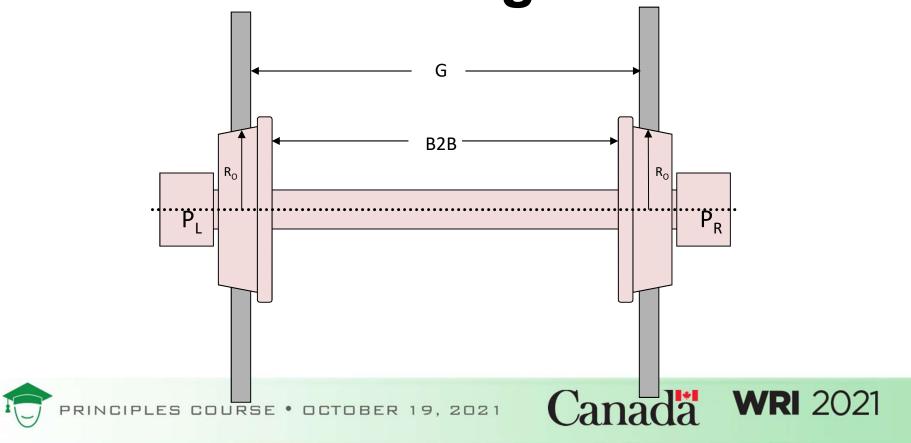


WHEELSET & VEHICLE **STEERING**

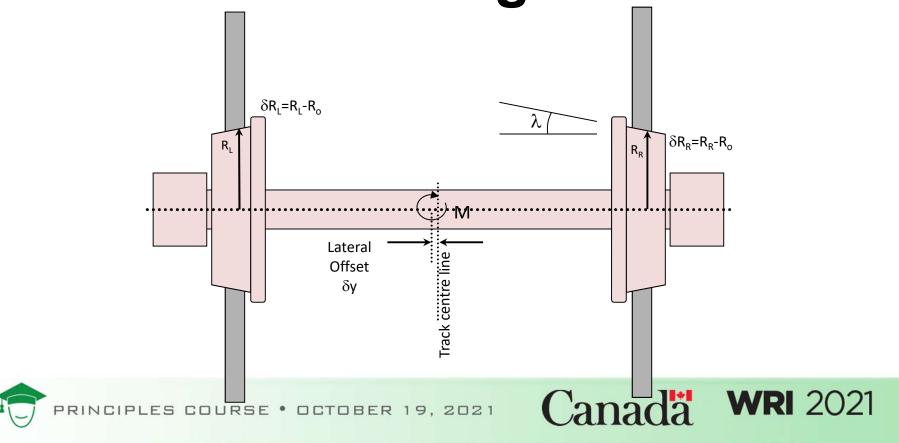




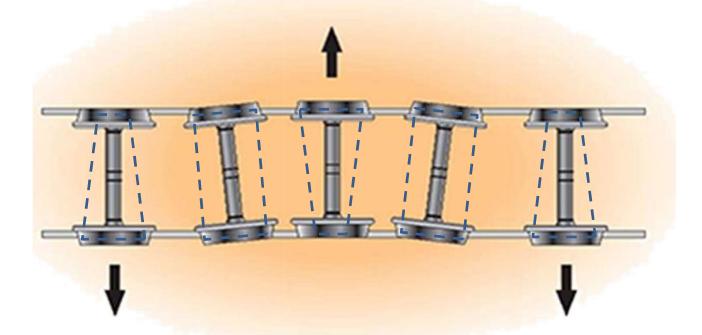
The Free Rolling Wheelset



The Free Rolling Wheelset



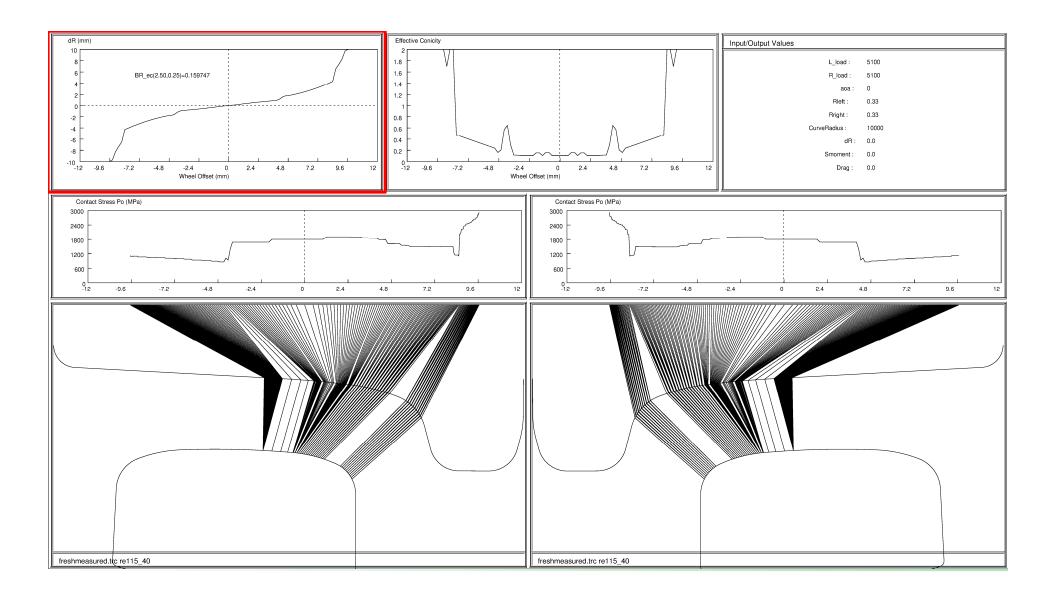
The Free Wheelset - Hunting







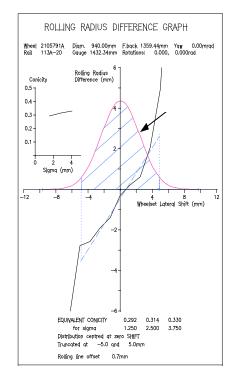




Equivalent Conicity from the ∆R Plot

British Rail derivation

$$\lambda_e = \frac{1}{2} \int \frac{N(y) (r_R - r_L)}{y} dy$$

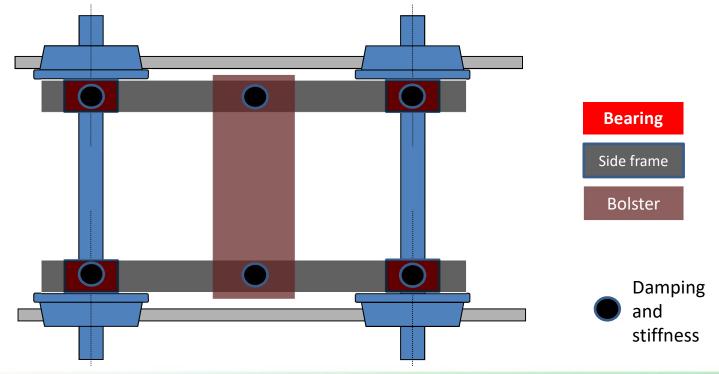








A Truck can Provide Stability



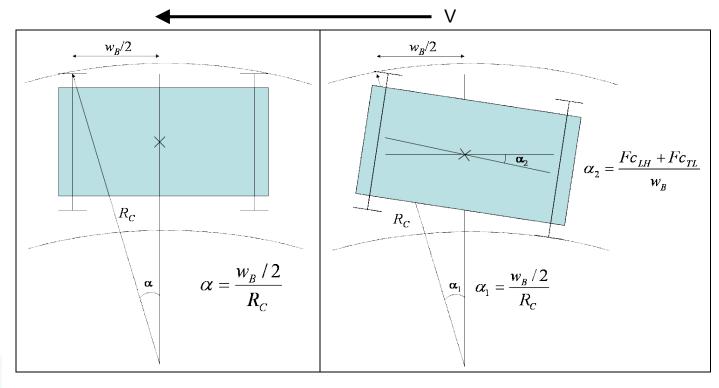






Leading Wheelset - Yaw Angle

- Rigid truck
- Self-steering (flexible)
- Steered



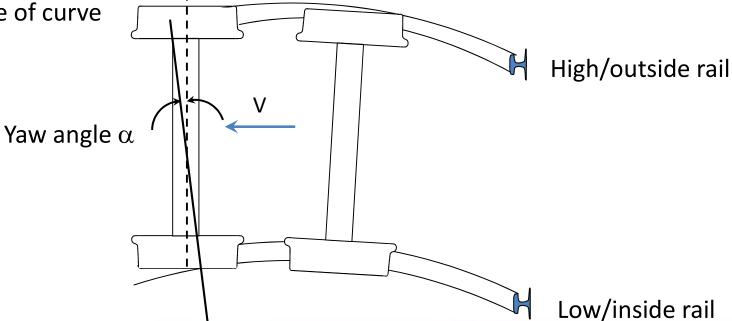


Also, yaw angle due to deflection of suspension (bending and shear)

The Wheelsets (in a curve)

(Leading) wheelset shifts

to outside of curve

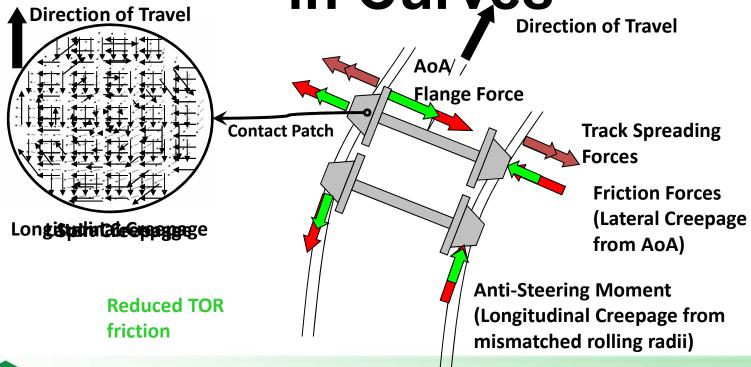








Lateral Forces (Creep) in Curves



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WHEEL-RAIL PROFILE DESIGN AND PERFORMANCE





Design of Engineered Rail Profiles

Rail design considers:

- Track curvature
- Worn wheel shapes
- Types of vehicle and speed (hunting)
- Dynamic rail rotation
- Rail hardness

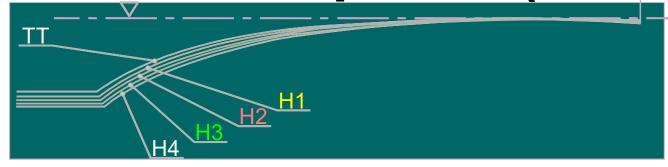
- control contact stress
- inhibit hunting
- minimize wear
- Grinding interval (profile deterioration between intervals)
- Static gage

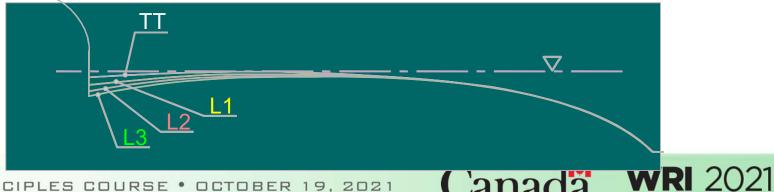






The NRC Family of Heavy Haul Rail Templates (1990s)









Rail Profile Design Criteria

Goals are to reduce/control:

- Gauge face and TOR wear
- Rolling contact fatigue (RCF)
- Dynamic instability (hunting)
- Corrugation formation
- Wheel hollowing

And are easily or practically implemented by grinding





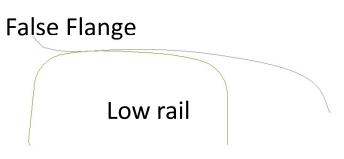


Wheel-Rail Contact Stresses

- Stress and damage depend on:
 - wheel radius
 - wheel load
 - friction coefficient
 - wheel/rail profiles (contact geometry)



Severe gauge-corner contact



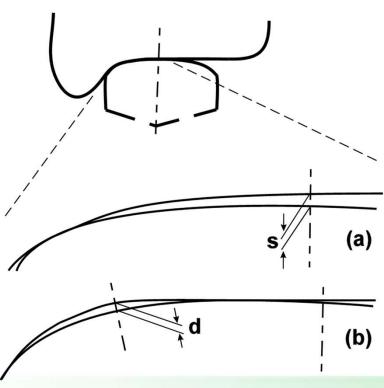
Hollow wheels







Wheel / Rail Conformality



- closely conformal0.1 mm (0.004") or less
- conformal0.1 mm to 0.4mm(0.004" to 0.016")
- non-conformal0.4 mm (0.016") or larger





Some Typical Issues Associated with Wheel/Rail Conformality

Closely conformal profiles

Dynamic instability (hunting)

Corrugation formation by spin creepage

Conformal profiles

Low stress state W/R interface

Used for mass transit and high speed lines = 1PT conformal

(good for steering)

Heavy haul = 2PT conformal (balance contact stress steering and wear)

Non-conformal profiles

High stress state W/R interface

1PT: cracks (RCF) at GC of HR and FS of LR

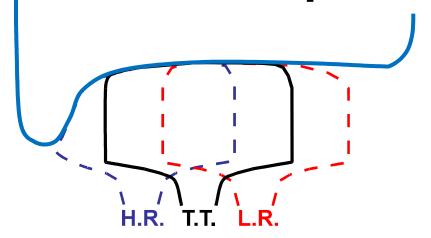
2PT: high gauge face wear in curves



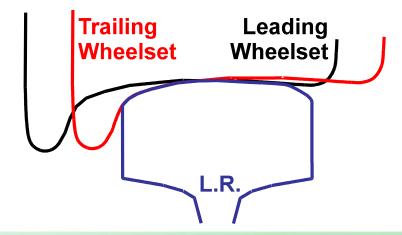




Worn Wheel and Rail Profiles are Envelopes of Each Other



 Worn wheel is an envelope of all rail profiles it encounters on a particular route Worn rail is an envelope of all wheel profiles that pass over it









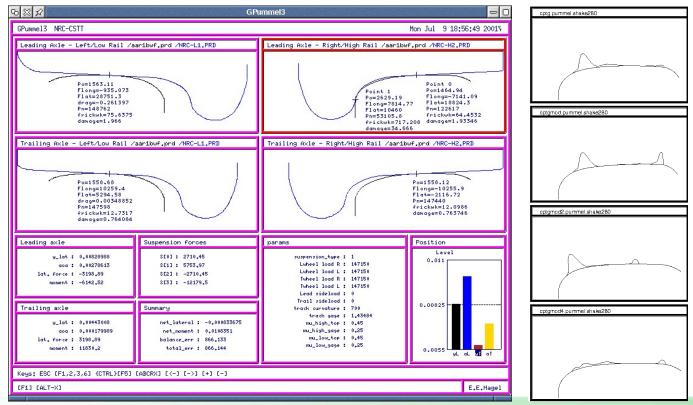
Pummelling Analysis

- Simulation
 - measured wheel profiles
 - vehicle characteristics (stiffness, wheelbase etc.)
 - rail hardness (for damage evaluation)
 - rail curvature, super-elevation, dynamic rail rotation etc.
- Evaluate distributions of
 - contact stress
 - steering moments
 - effective conicity





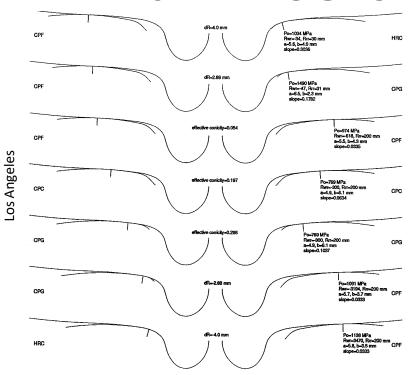
Pummelling: Design/Analysis Tool²³

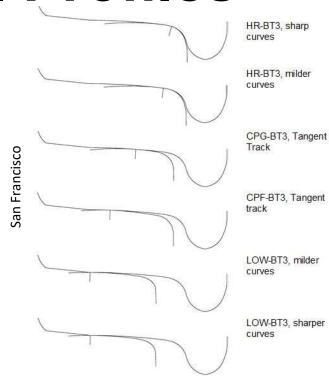






Families of Rail Profiles











VTI DERAILMENT MECHANISMS AND RISK **ASSESSMENT**

- Wheel climb
- Low rail rollover





WHEEL CLIMB

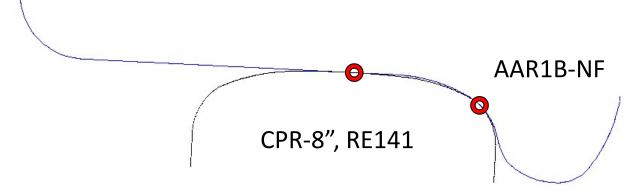






Wheel/Rail Contact

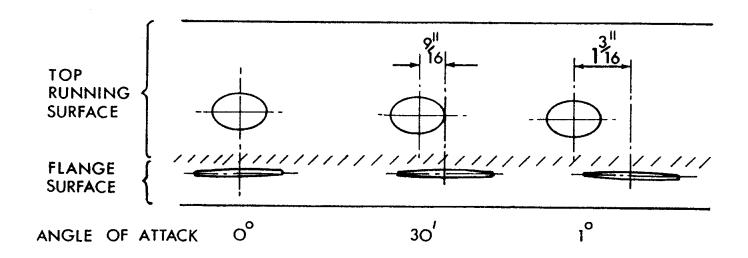
 W/R contact often takes place at two points simultaneously (some new wheels especially)







Wheel/Rail Contact (cont'd)



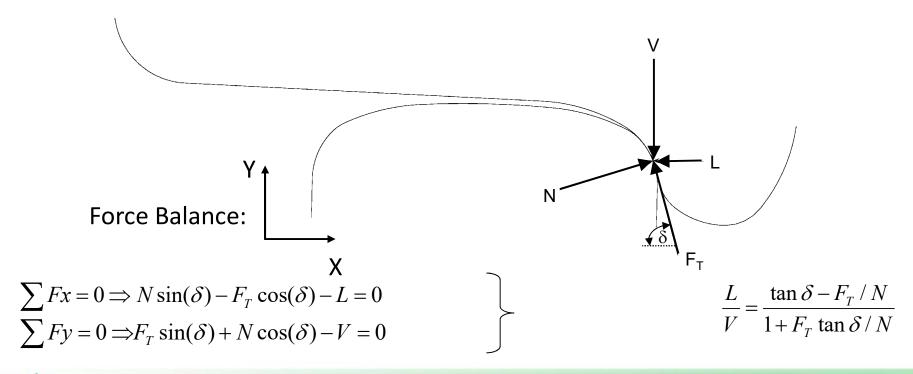
Plan view of contact ellipses on high rail for different angles of attack







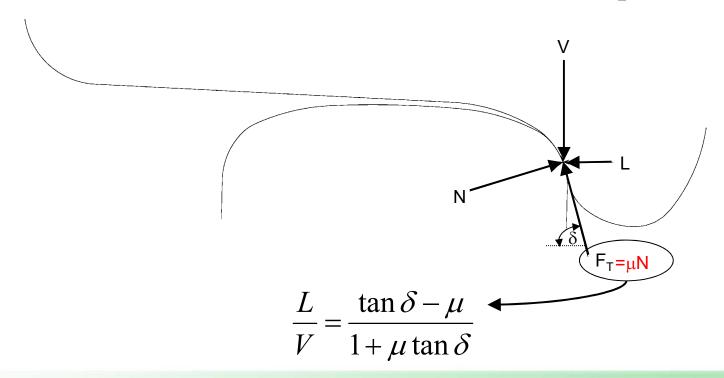
Deriving Nadal







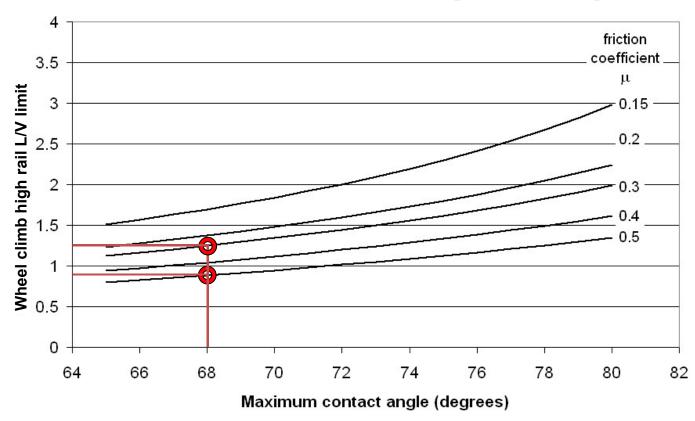
Nadal's Relationship





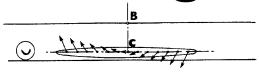


Nadal Index (1908)

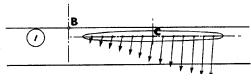




Slip Vectors at the Gage Face Contact



$$\delta > \beta$$
, $\alpha = 0$

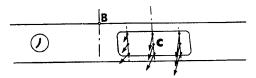


 $\delta < \beta$, large α



 δ = wheel flange angle

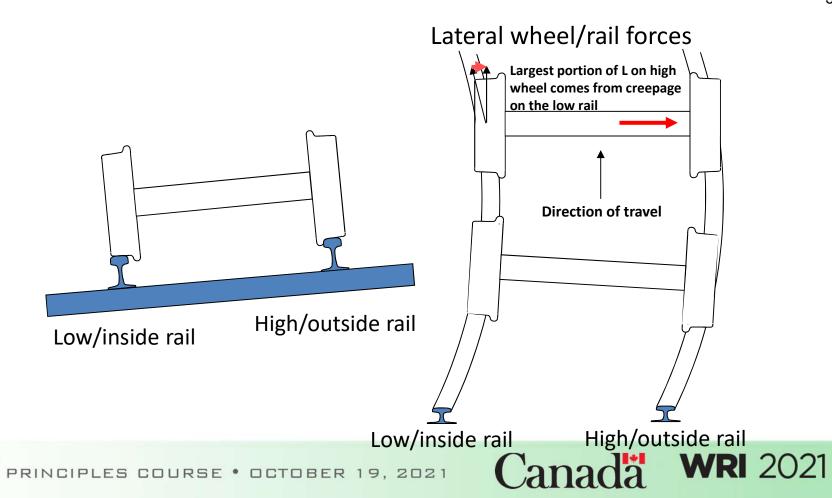
 β = gage face angle



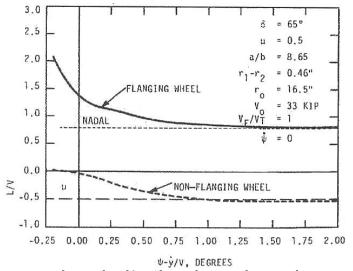
 δ =β, moderate α







Weinstock Derailment Criterion



$$|L/V|_{flanging} + |L/V|_{non_flanging} >$$

 $(L/V_{NADAL} + m)$

- Holds for all positive angles of attack,
- Less accurate for +ve cant deficiency

 At incipient wheel climb, the L/V values on the flanging and non-flanging wheels are, for positive angles of attack, separated by a roughly constant value equal to the Nadal limit plus the coefficient of friction on the top of the low rail

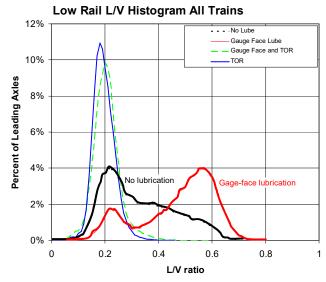
21

Canada

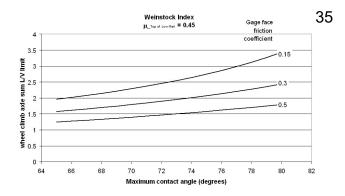
WRI 2021

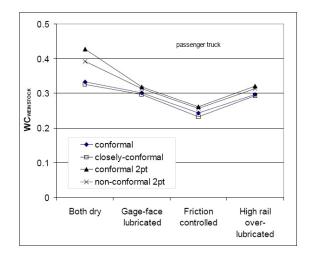
An Example

• Is lubrication a good thing?



L/V goes up, but Weinstock limit also.











Wheel Climb - Conclusions

- Nadal provides a relationship between contact angle and friction coefficient
- Is based upon simplified view of the slip conditions
- Wheel climb threshold matches Nadal at most practical angles of attack, but not for low aoa.
- Weinstock rectifies that (for positive angles of attack) and includes explicitly the effect of friction on top of low rail.
- A safe L/V is some fraction of the (Nadal or Weinstock) threshold value, say 60-80%.
- These are static and quasi-static derivations.





LOW RAIL ROLLOVER

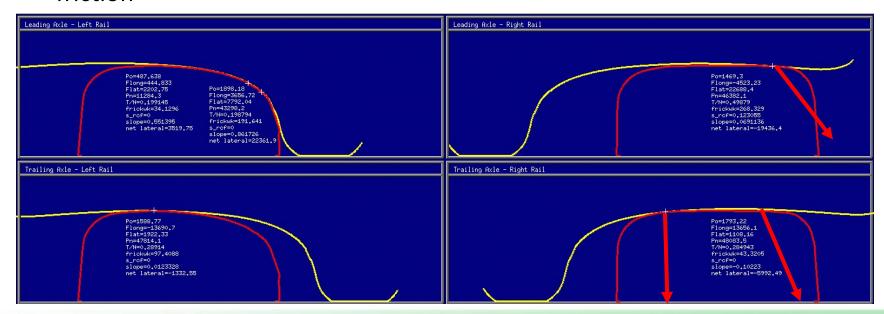






Low Rail Rollover

Wide gauge, hollow wheels, poor restraint, underbalanced running, high friction









Conclusions

- Matching of wheel/rail profiles
 - Rolling radius difference: stability and curving
 - Strong impact on stress, curving forces, stability, surface damage,
 safety/derailment (with friction conditions, truck suspensions, track geometry etc.)
 - Must consider both new and worn shapes (pummeling)
- Nadal formula is adequate for most wheel climb analyses



